# A33230

# 3D Hall-Effect Sensor IC with Sine/Cosine Outputs

## FEATURES AND BENEFITS

- 5 V supply voltage
- Tiny SOT23-W
- Pre-programmed axis combinations: XY, XZ, or YZ
- Ratiometric outputs
- Low output current
- Two selectable sensitivities
- AEC-Q100 grade 0 automotive qualified
- Quality managed (QM)

## PACKAGE:

**5-Pin SOT23-W (Suffix LH)**



*Not to scale*

## DESCRIPTION

The A33230 is an integrated circuit (IC) 3D Hall-effect sensor IC intended for position sensing of magnet targets. The IC incorporates vertical and planar Hall-effect elements with sensing axes that are orthogonal to one another, providing 90° phase separation. This phase separation is inherently independent of magnet pole spacing and air gap.

The IC comes pre-programmed to XY, XZ, or YZ combinations while providing independent sine and cosine outputs. User-defined linearization and error compensation may be required.

The A33230 is provided in a 5-pin SOT23-W package (suffix LH). The package is RoHS compliant and lead (Pb) free with a 100% matte-tin leadframe plating.

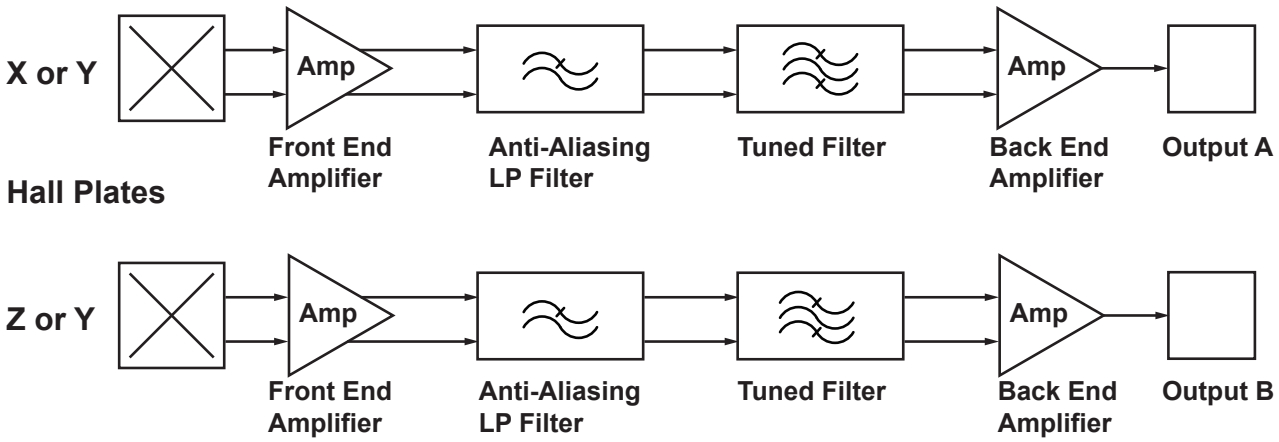



**Figure 1: Functional Block Diagram**

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## SELECTION GUIDE

| Part Number | Application | | Number of Die | Package | Packing |
|---|---|---|---|---|---|
| A33230LLHALT-XY-S-AR-03 | XY | 300 G | Single | 5-pin SOT23-W (suffix LH) | 3000 pieces per 7-inch reel |
| A33230LLHALT-XY-S-AR-10 | | 1000 G | | | |
| A33230LLHALT-XZ-S-AR-03 | XZ | 300 G | | | |
| A33230LLHALT-XZ-S-AR-10 | | 1000 G | | | |
| A33230LLHALT-YZ-S-AR-03 | YZ | 300 G | | | |
| A33230LLHALT-YZ-S-AR-10 | | 1000 G | | | |

[1] For other package options, contact Allegro.

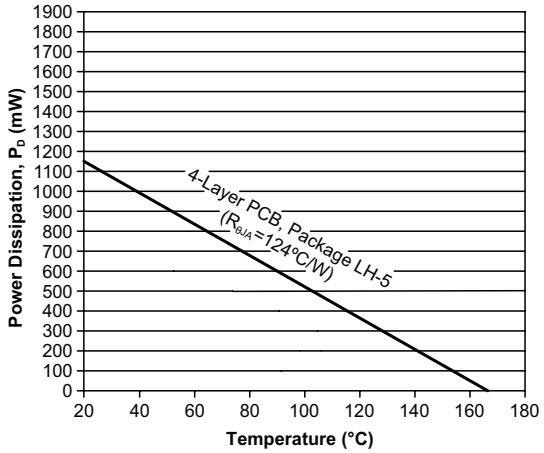
## ABSOLUTE MAXIMUM RATINGS

| Characteristic | Symbol | Notes | Rating | Unit |
|---|---|---|---|---|
| Forward Supply Voltage | $V_{CC}$ | | 7 | V |
| Reverse Supply Voltage | $V_{RCC}$ | | –0.1 | V |
| Forward Output Voltage | $V_{OUT}$ | | 7 | V |
| Reverse Output Voltage | $V_{ROUT}$ | | –0.1 | V |
| Output Source Current | $I_{OUT(SOURCE)}$ | VOUT to GND | 1 | mA |
| Output Sink Current | $I_{OUT(SINK)}$ | VCC to VOUT | 10 | mA |
| Operating Ambient Temperature | $T_A$ | | –40 to 150 | °C |
| Maximum Junction Temperature | $T_{J(max)}$ | | 165 | °C |
| Storage Temperature | $T_{stg}$ | | –65 to 170 | °C |

## THERMAL CHARACTERISTICS: May require derating at maximum conditions; see application information

| Characteristic | Symbol | Test Conditions* | Value | Unit |
|---|---|---|---|---|
| Package Thermal Resistance | $R_{\theta JA}$ | Package LH-5 4-layer PCB based on JEDEC standard JESD51-7 | 124 | °C/W |

*Additional thermal information available on the Allegro website.

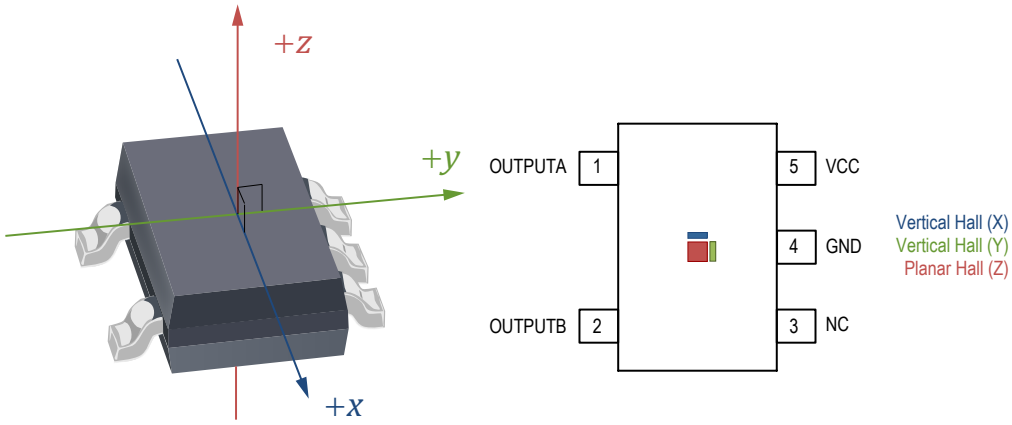



**Maximum Power Dissipation versus Ambient Temperature**



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## PINOUT DIAGRAM AND LIST




**LH-5 Package Pinouts**

**Pinout List**

| Number | Name | Function |
|---|---|---|
| 1 | OUTPUTA | Cosine/Sine Output |
| 2 | OUTPUTB | Cosine/Sine Output |
| 3 | NC | Not Connected (Connect to GND for optimal EMC performance) |
| 4 | GND | Ground |
| 5 | VCC | Supply Voltage |

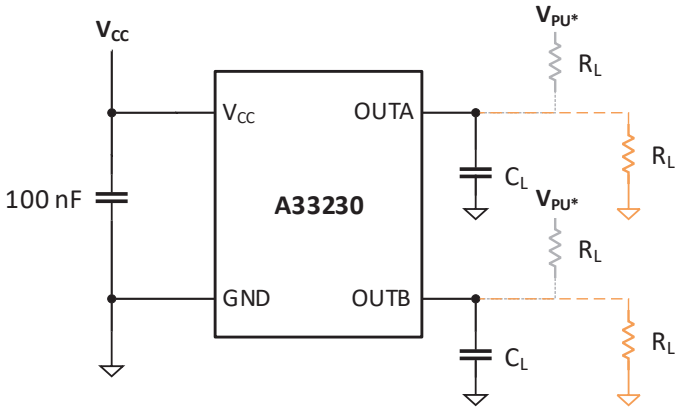



**Figure 2: Typical Application Circuit**

The load capacitance is optional for best noise performances. Typical value for $C_L$ is 1 nF.
The load resistors are also optional with a pull-up configuration (gray) or a pull-down configuration (orange).
* $V_{PU} \leq V_{CC}$



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**OPERATING CHARACTERISTICS:** Valid over operating voltage and temperatures, unless otherwise specified

| Characteristics | Symbol | Test Conditions | | Min. | Typ. [1] | Max. | Unit |
|---|---|---|---|---|---|---|---|
| **ELECTRICAL SUPPLY CHARACTERISTICS** | | | | | | | |
| Supply Voltage | $V_{CC}$ | | | 4.5 | 5.0 | 5.5 | V |
| Supply Current | $I_{CC}$ | No load | | – | 7.0 | 10 | mA |
| Output Source Current | $I_{SOURCE}$ | $R_L$ = 8 kΩ | | – | 0.5 | – | mA |
| Output Sink Current | $I_{SINK}$ | $R_L$ = 8 kΩ | | – | 0.5 | – | mA |
| **ELECTRICAL PROTECTION CHARACTERISTICS** | | | | | | | |
| Supply Zener Clamp Voltage | $V_{ZSUPPLY}$ | $I_{CC} = I_{CC(MAX)} + 5$ mA | | 7 | – | – | V |
| Reverse Supply Zener Clamp Voltage | $V_{RZSUPPLY}$ | $I_{CC}$ = –1 mA | | – | – | –0.1 | V |
| **POWER-ON STATE CHARACTERISTICS** | | | | | | | |
| Power-On Time [2] | $t_{PO}$ | Time from $V_{CC} \geq V_{CC}$(min) to when OUTPUTA and OUTPUTB are >90% of steady-state value | | – | 25 | 60 | µs |
| **OUTPUT CHARACTERISTICS** | | | | | | | |
| Voltage Range [2] | $V_{OUT(SAT)HIGH}$ | $I_{OUT}$ = 550 µA | | $V_{CC}$ – 0.5 | – | – | V |
| | $V_{OUT(SAT)LOW}$ | $I_{OUT}$ = –550 µA | | – | – | 0.5 | V |
| Input Magnetic Flux Density [2][3] | B | 1000 G option | | – | 1000 | 1200 | G |
| | | 300 G option | | – | 300 | 400 | G |
| Quiescent Voltage Output (QVO) | $V_{OUT(Q)}$ | | | – | $V_{CC}$ / 2 | – | V |
| QVO Error | $V_{ERROUT(Q)}$ | $T_A$ = 25°C | | –70 | – | 70 | mV |
| | | $T_A$ = –40°C to 150°C | | –125 | – | 125 | mV |
| Sensitivity | Sens | $V_{CC}$ = 5 V [4], 1000 G option, $T_A$ = 25°C | | 0.9 | 1.2 | 1.5 | mV/G |
| | | $V_{CC}$ = 5 V [4], 300 G option, $T_A$ = 25°C | | 2.7 | 3.6 | 4.5 | mV/G |
| Sensitivity Mismatch | $MM_{SENS}$ | $(Sens_B – Sens_A) / Sens_A \times 100\%$ | | – | ±3 | – | % |
| Orthogonality Error | OG | Phase difference between sine and cosine signals ($OG = \varphi_C – \varphi_S$) | | – | ±1 | – | degrees |
| Input Referred Noise Density | σ | OUTA and OUTB, 1σ | $T_A$ = 25°C | – | 4.5 | – | $mG_{rms}/\sqrt{Hz}$ |
| | | | $T_A$ = 150°C | – | 8.25 | – | $mG_{rms}/\sqrt{Hz}$ |
| Output Effective Resolution | ER | \|B\| = 1000 G, 1σ, BW = 50 kHz | $T_A$ = 25°C | – | 11 | – | bits |
| | | | $T_A$ = 150°C | – | 10 | – | bits |
| | | \|B\| = 300 G, 1σ, BW = 50 kHz | $T_A$ = 25°C | – | 9 | – | bits |
| | | | $T_A$ = 150°C | – | 8 | – | bits |
| Slew Rate [5] | SR | $C_L$ = 5 nF | | 100 | – | – | kV/s |
| Response Time [5] | $t_R$ | Time from input magnetic sinusoidal stimulus to output response; BW = 50 kHz | | – | 6.7 | – | µs |
| Bandwidth [5] | BW | | | 35 | 50 | 75 | kHz |

[1] Typical values at $V_{CC}$ = 5 V and $T_A$ = 25°C, unless otherwise specified. Performance may vary for individual units, within the minimum and maximum limits.
[2] Specification is guaranteed by design and characterization.
[3] Input Magnetic Flux Density can exceed the maximum limit presented in the table without damaging the device. Device channel linearity error will deteriorate if the limit is exceeded.
[4] Sensitivity of the device will change with $V_{CC}$ because the output is ratiometric. If $V_{CC}$ is different from 5 V, use the following equation to solve for the sensitivity: $Sens_{(VCC)} = Sens_{(5V)} \times V_{CC} / 5$ V.
[5] Specification is guaranteed by design.

*Continued on next page...*

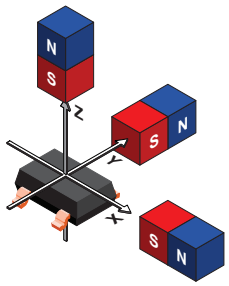


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**OPERATING CHARACTERISTICS (continued):** Valid over operating voltage and temperatures, unless otherwise specified

| Characteristics | Symbol | Test Conditions | | Min. | Typ. [1] | Max. | Unit |
|---|---|---|---|---|---|---|---|
| **ACCURACY PERFORMANCE** | | | | | | | |
| Channel Linearity Error | $ERR_{LIN}$ | Error of device output relative to an ideal output; $\|B_{APPLIED}\| \le \|B_{MAX}\|$ | | –0.3 | – | 0.3 | % |
| Offset Ratiometry Error | $ERR_{RAT(QVO)}$ | Error of $V_{OUT(Q)}$ relative to a perfectly ratiometric response for $V_{CC}$ = 5 V ±0.5 V, relative to 5 V | | –1 | – | 1 | % |
| Sensitivity Ratiometry Error | $ERR_{RAT(SENS)}$ | Error of Sens relative to a perfectly ratiometric response for $V_{CC}$ = 5 V ±0.5 V, relative to 5 V | | –5 | – | 5 | % |
| Angle Micro-Linearity Error | $ERR_{\mu LIN(\theta)}$ | Over 1° input range; \|B\| = 300 G; Typ. = 3 σ | | – | ±0.15 | – | degrees |
| **ANGLE PERFORMANCE** | | | | | | | |
| Native Angle Error [2][3][4] | $ERR_{ANG(NAT,300)}$ | No Correction [6], RPM = 0 | Valid for \|B\| = 300 G | –6.1 | ±2.2 | 6.1 | degrees |
| | $ERR_{ANG(NAT,1000)}$ [5] | | Valid for \|B\| = 1000 G | –3.3 | ±1.2 | 3.3 | degrees |
| One Time External Correction [2][3][4] | $ERR_{ANG(OT,300)}$ | Ideal External Offset, Amplitude, and Phase correction at $T_A$ = 25°C, RPM = 0 | Valid for \|B\| = 300 G | –5.1 | ±1.8 | 5.1 | degrees |
| | $ERR_{ANG(OT,1000)}$ [5] | | Valid for \|B\| = 1000 G | –2.9 | ±1.0 | 2.9 | degrees |
| Dynamic External Correction [2][3][4] | $ERR_{ANG(DYN)}$ | Ideal External Phase correction at $T_A$ = 25°C with Cycle-by-Cycle Offset and Amplitude Correction; RPM = 0 | Valid for both \|B\| = 300 G and \|B\| = 1000 G | –0.7 | ±0.2 | 0.7 | degrees |
| Harmonic Distortion Error | $ERR_{ANG(HD)}$ | Resulting Error after Ideal External Offset, Amplitude, and Phase Correction; RPM = 0 | | – | ±0.2 | – | degrees |
| Angle Noise [7] | σθ | \|B\| = 1000 G | $T_A$ = 25°C | – | 0.07 | – | °RMS |
| | | | $T_A$ = 150°C | – | 0.13 | – | °RMS |
| | | \|B\| = 300 G | $T_A$ = 25°C | – | 0.24 | – | °RMS |
| | | | $T_A$ = 150°C | – | 0.44 | – | °RMS |
| Angle Effective Resolution [7] | $ER_{\theta}$ | $Log_2(360/\sigma\ \theta)$, \|B\| = 1000 G | $T_A$ = 25°C | – | 12 | – | bits |
| | | | $T_A$ = 150°C | – | 11 | – | bits |
| | | $Log_2(360/\sigma\ \theta)$, \|B\| = 300 G | $T_A$ = 25°C | – | 10 | – | bits |
| | | | $T_A$ = 150°C | – | 9 | – | bits |
| **OUTPUT REQUIREMENTS** | | | | | | | |
| Output Load Capacitance [8] | $C_L$ | Capacitance between each output and ground | | 0 | – | 5 | nF |
| Output Load Resistance [8] | RL | Resistance between each output and ground | | 8 | – | ∞ | kΩ |

[1] Typical values at $V_{CC}$ = 5.0 V and $T_A$ = 25°C, unless otherwise specified. Performance may vary for individual units, within the minimum and maximum limits.
[2] The angle accuracy depends on the magnetic system, calibration procedure, and the compensation method of the ECU.
[3] Parameters are valid over operating temperature and operating voltage. A total population of 180 devices consisting of three unique wafer fabrication lots were used.
[4] Specification maximum value is equal to the mean of the absolute maximum angle error plus three sigma. This value is determined by characterization.
[5] Specification maximum value is interpolated based off silicon evaluation measurements. This value is determined by characterization.
[6] Native Angle Error specification assumes both voltage outputs are reduced by $V_{CC}$/2 for the arctangent CORDIC calculation.
[7] Theoretical value derived from the output referred noise.
[8] Specification is guaranteed by design.




**South polarity magnetic fields, in the orientations illustrated (above), are considered positive fields.**



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## CHARACTERISTIC PLOTS

### Offset Error

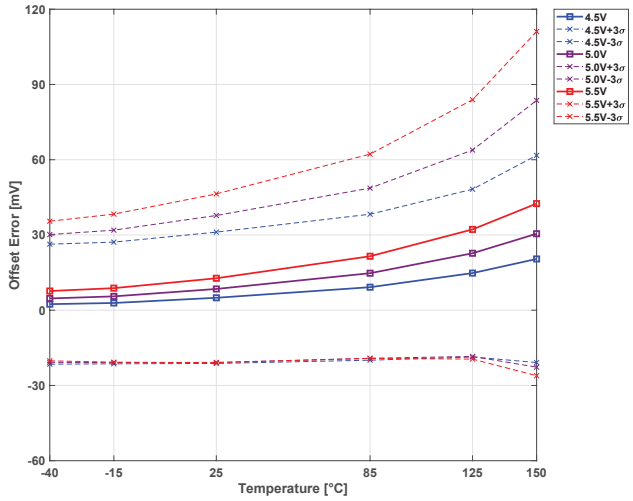



**Figure 3: Average X,Y Offset Error ±3σ over Temperature and $V_{CC}$**

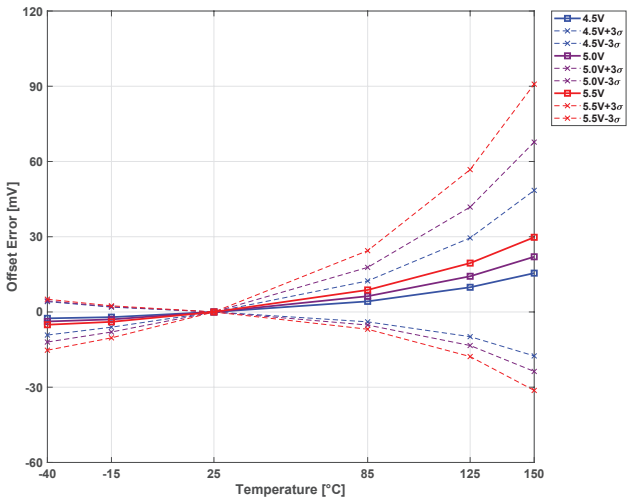



**Figure 4: Average X,Y Offset Error Temperature Drift ±3σ over Temperature and $V_{CC}$**

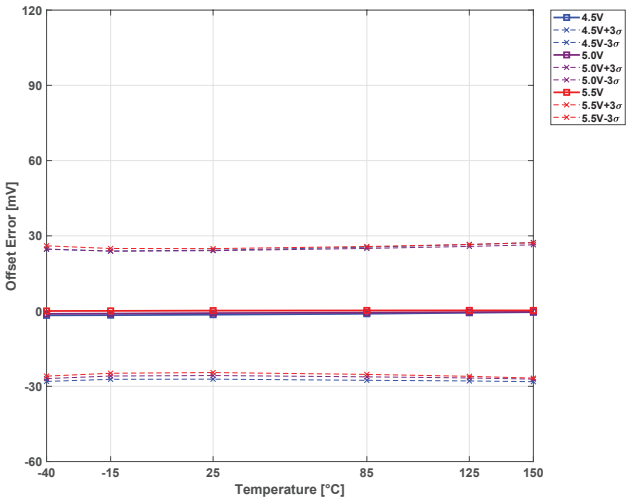



**Figure 5: Average Z Offset Error ±3σ over Temperature and $V_{CC}$**

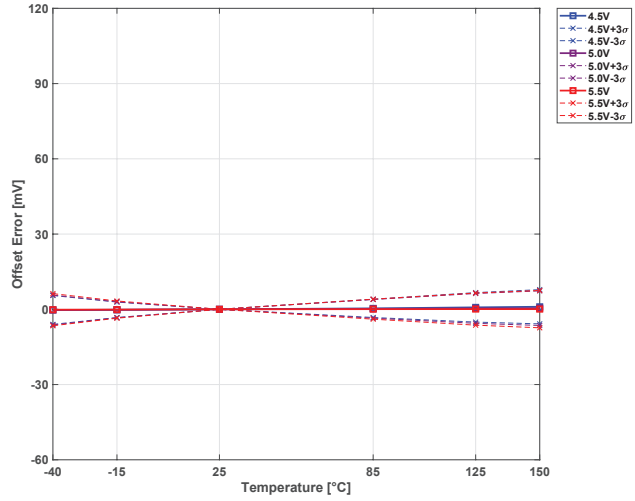



**Figure 6: Average Z Offset Error Temperature Drift ±3σ over Temperature and $V_{CC}$**



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## CHARACTERISTIC PLOTS (continued)

### Sensitivity

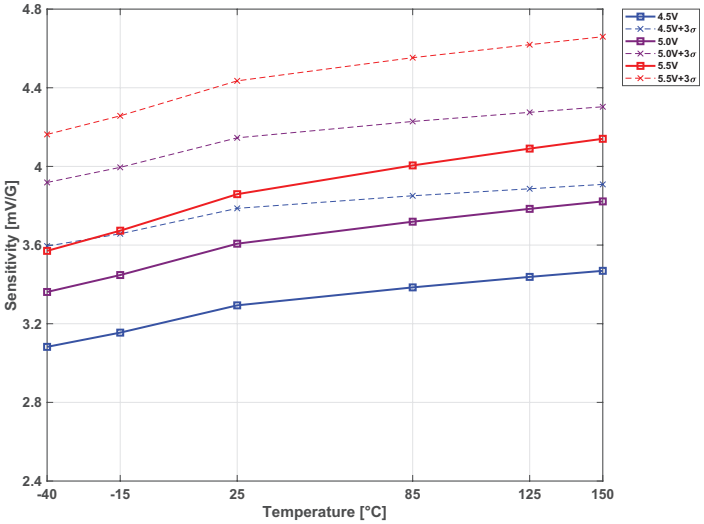



Figure 7: 300 G Option, Average Sensitivity +3σ over Temperature and $V_{CC}$

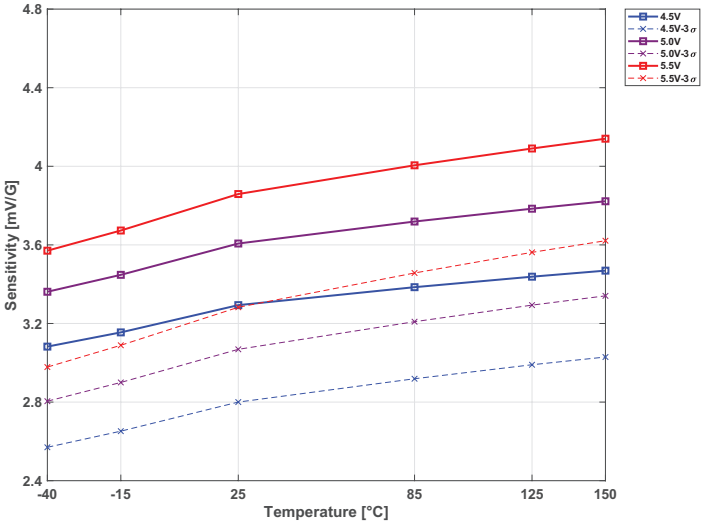



Figure 8: 300 G Option, Average Sensitivity -3σ over Temperature and $V_{CC}$

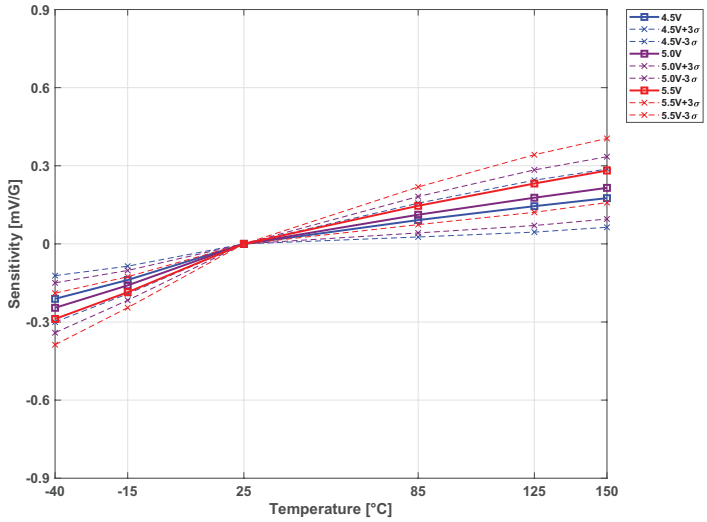



Figure 9: 300 G Option, Average X,Y Sensitivity Temperature Drift +3σ over Temperature and $V_{CC}$

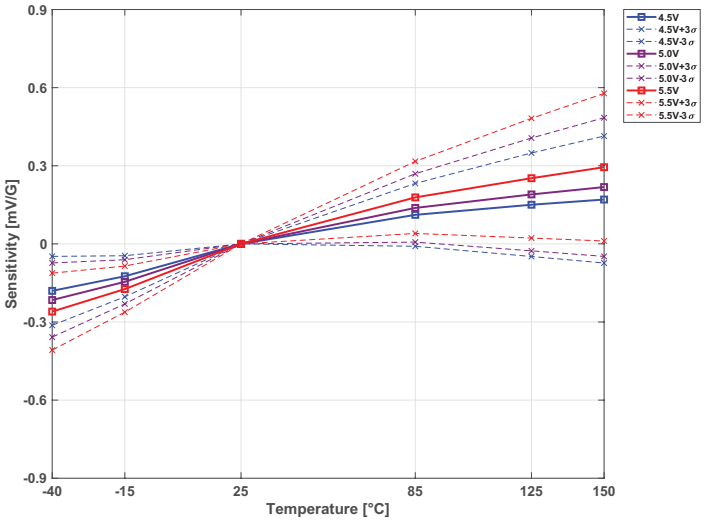



Figure 10: 300 G Option, Average Z Sensitivity Temperature Drift +3σ over Temperature and $V_{CC}$



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## CHARACTERISTIC PLOTS (continued)

### Angle Performance

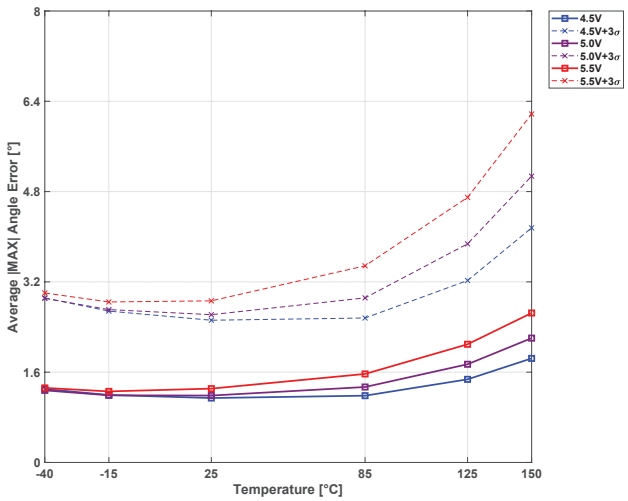



**Figure 11: Average |Max| Native Angle Error +3σ over Temperature and $V_{CC}$**

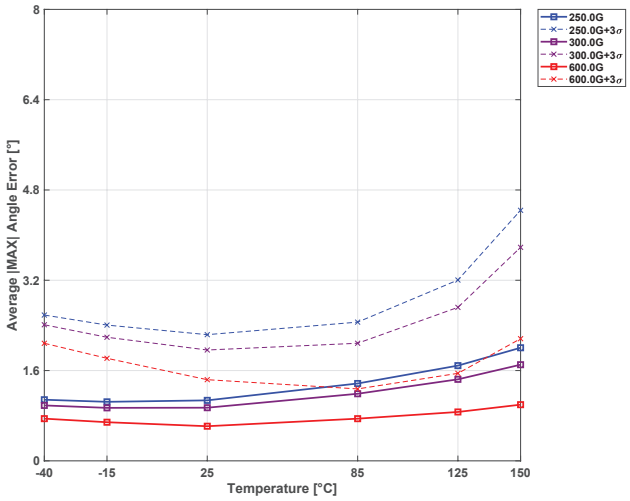



**Figure 12: 300 G Option, Average |Max| Native Angle Error +3σ over Temperature and Field [1]**

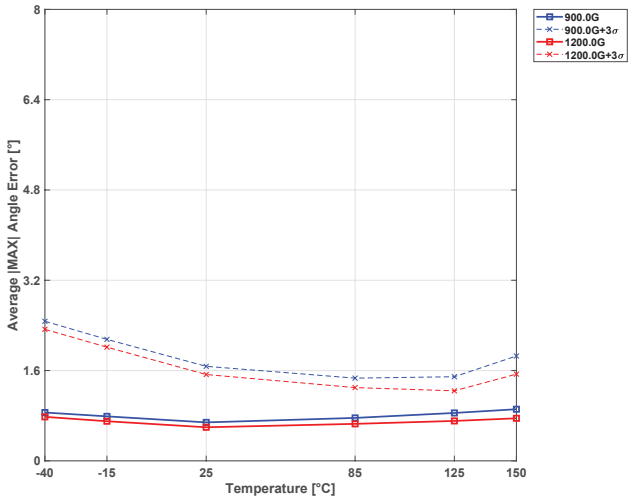



**Figure 13: 1000 G Option, Average |Max| Native Angle Error +3σ over Temperature and Field [1]**

[1] The data represented in Figure 12 and Figure 13 is meant to show a characteristic trend in behavior over magnetic field, not to guarantee performance by characterization.



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## CHARACTERISTIC PLOTS (continued)

### Angle Performance (continued)

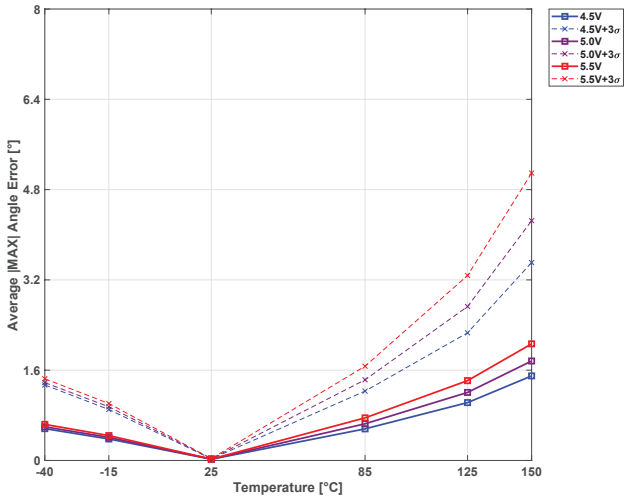



**Figure 14: Average |Max| One Time Correction Angle Error +3σ over Temperature and $V_{CC}$**

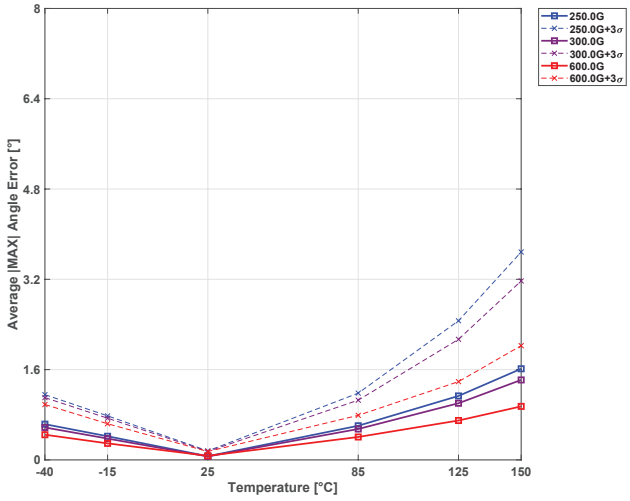



**Figure 15: 300 G Option, Average |Max| One Time Correction Angle Error +3σ over Temperature and Field [1]**

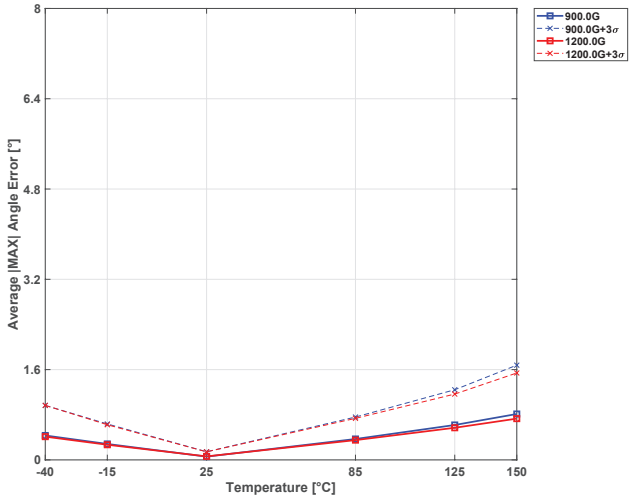



**Figure 16: 1000 G Option, Average |Max| One Time Correction Angle Error +3σ over Temperature and Field [1]**

[1] The data represented in Figure 15 and Figure 16 is meant to show a characteristic trend in behavior over magnetic field, not to guarantee performance by characterization.



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## CHARACTERISTIC PLOTS (continued)

### Angle Performance (continued)

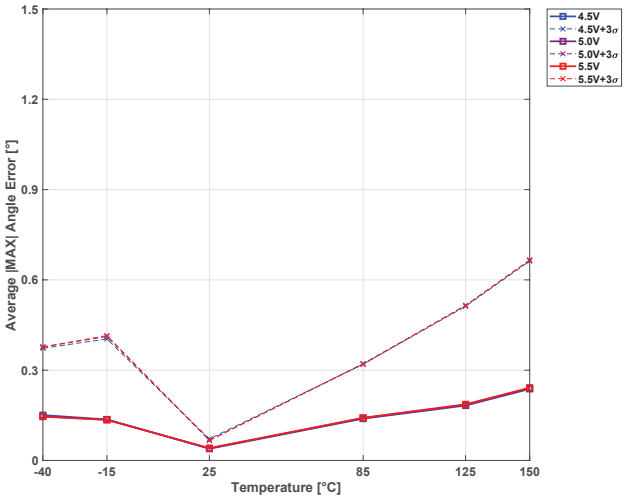



**Figure 17: Average |Max| Dynamic Correction Angle Error +3σ over Temperature and $V_{CC}$**



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## CHARACTERISTIC DEFINITIONS

### Quiescent Voltage Output

In the quiescent state (no significant magnetic field: B = 0 G), the output, $V_{OUT(Q)}$, is at a constant ratio to the supply voltage, $V_{CC}$, across the entire operating ranges of $V_{CC}$ and Operating Ambient Temperature, $T_A$. The ideal quiescent state output is $V_{CC}$ / 2, so any deviations between $V_{OUT(Q)}$ and $V_{CC}$ / 2 is QVO Error, $V_{ERROUT(Q)}$.

Equation 1:

$$V_{ERROUT(Q)} = (V_{OUT(Q)} - \frac{V_{CC}}{2})$$

### QVO Temperature Drift

As operating temperature changes, $V_{OUT(Q)}$ will drift. $V_{OUT(Q)(TC)}$ is meant to describe this behavior relative to $V_{OUT(Q)}$ at 25°C expressed in Equation 2 as:

Equation 2:

$$V_{OUT(Q)(TC)} = \frac{V_{OUT(Q)(T_A)} - V_{OUT(Q)(25°C)}}{T_A - 25°C}$$

### Sensitivity

The amount of the output voltage change is proportional to the magnitude and polarity of the magnetic field applied. This proportionality is specified as the magnetic sensitivity, Sens (mV/G), of the device and is defined in Equation 3:

Equation 3:

$$Sens = \frac{V_{OUT(B+)} - V_{OUT(B-)}}{(B+) - (B-)}$$

where B+ is the magnetic flux density in a positive field (south polarity) and B– is the magnetic flux density in a negative field (north polarity). The sensitivity of the device will change with a change in $V_{CC}$, so use the equation in footnote 4 on page 4.

### Sensitivity Temperature Drift

As operating temperature changes, the sensitivity of the device will change. $SENS_{TC}$ is meant to describe this behavior relative to SENS at 25°C, expressed in Equation 4 as:

Equation 4:

$$Sens_{TC} = \frac{Sens_{(T_A)} - Sens_{25°C}}{T_A - 25°C}$$

### Sensitivity Error

The A33230 is designed to provide linear outputs in response to a ramping applied magnetic field. Consider two magnetic fields, B1 and B2. Ideally, the sensitivity of a device is the same for both fields for a given supply voltage and temperature. Sensitivity error is present when there is a difference between the sensitivities measured at B1 and B2.

Sensitivity Error, $Sens_{ERR}$, is calculated separately for positive ($Sens_{ERR+}$) and negative ($Sens_{ERR-}$) applied magnetic fields. $Sens_{ERR}$ (%) is measured and defined as follows:

Equation 5:

$$Sens_{ERR+} = \left(1 - \frac{Sens_{(B2+)}}{Sens_{(B1+)}}\right) \times 100\ (\%)$$

$$Sens_{ERR-} = \left(1 - \frac{Sens_{(B2-)}}{Sens_{(B1-)}}\right) \times 100\ (\%)$$

where

Equation 6:

$$Sens_{Bx} = \frac{|V_{OUT(Bx)} - V_{OUT(Q)}|}{B_x}$$

### Channel Linearity Error

Channel linearity error, $ERR_{LIN}$, quantifies the deviation of OUTPUTA/B over an applied magnetic field relative to a perfect line. The ideal $V_{OUT}$ of the device is comprised of the Applied Field ($B_A$) multiplied by the device's sensitivity (Sens) plus the device's Offset ($V_{OUT(Q)}$). This is expressed in Equation 7 as:

Equation 7:

$$ERR_{LIN} = \frac{V_{OUT(B_A)} - (B_A \times Sens + V_{OUT(Q)})}{|B_A \times Sens + V_{OUT(Q)}|} \times 100\%$$

The device will provide a linear output within specification for any $B_A \leq B_{MAX}$. For $B_A > B_{MAX}$, channel linearity performance will no longer be guaranteed.

### Offset Ratiometry Error

Offset ratiometry error, $ERR_{RAT(QVO)}$, quantifies the non-linearity of OUTPUTA/B's offset ($V_{OUT(Q)}$) over a changing supply voltage when there is 0 G of applied magnetic field. This is expressed in Equation 8 below. $V_{OUT(Q)}$ will change with a change in $V_{CC}$.



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Equation 8:

$$ERR_{RAT(QVO)} = \left[ \frac{(V_{OUT(Q)(V_{CC})} - V_{OUT(Q)(5V)})}{V_{OUT(Q)(5V)}} - \frac{(V_{CC} - V_{CC(5V)})}{V_{CC(5V)}} \right] \times 100\%$$

## Sensitivity Ratiometry Error

Sensitivity ratiometry error, $ERR_{RAT(SENS)}$, quantifies the non-linearity of OUTPUTA/B's sensitivity over a changing supply voltage at a fixed magnetic field. This is expressed in Equation 9 below. Sens will change with a change in $V_{CC}$.

Equation 9:

$$ERR_{RAT(SENS)} = \left[ \frac{(Sens_{(V_{CC})} - Sens_{(5V)})}{Sens_{(5V)}} - \frac{(V_{CC} - V_{CC(5V)})}{V_{CC(5V)}} \right] \times 100\%$$

## Offset, Amplitude, Phase Correction, and Angle Derivation

The device provides sine and cosine signals whose argument is the local in-plane magnetic field angle. These signals are used downstream by the system for an angle derivation performed externally to the device. This section explains the typical angle derivation which includes offset, amplitude, and phase correction of the sinusoidal signals.

The two signals provided by the sensor are denoted x and y and can be modelled as follows:

$$\begin{cases} x(\theta) = A_c \cos(\theta + \varphi_c) + O_c \\ y(\theta) = A_s \sin(\theta + \varphi_s) + O_s \end{cases}$$

where $A_C$, $A_S$ are the amplitude of the cosine and sine signals,

$O_C$, $O_S$ are the offset of the cosine and sine signals, and

$\varphi_C$, $\varphi_S$ are the phase of the cosine and sine signals, with respect to an arbitrary angle reference.

The above parameters are typically obtained in a calibration step or learned dynamically during the operation of the device by an external system. The parameters can be derived at different fields and or temperatures. Contact Allegro for further information on how to derive these parameters.

Once the above list of parameters is available, the offset, amplitude, and phase correction can be applied on every new (x,y) samples simultaneously acquired from the sensor. The correction must be performed as follow:

Offset removal and amplitude normalization:

$$x_{norm} = \frac{x(\theta) - O_c}{A_c}, \qquad y_{norm} = \frac{y(\theta) - O_s}{A_s}$$

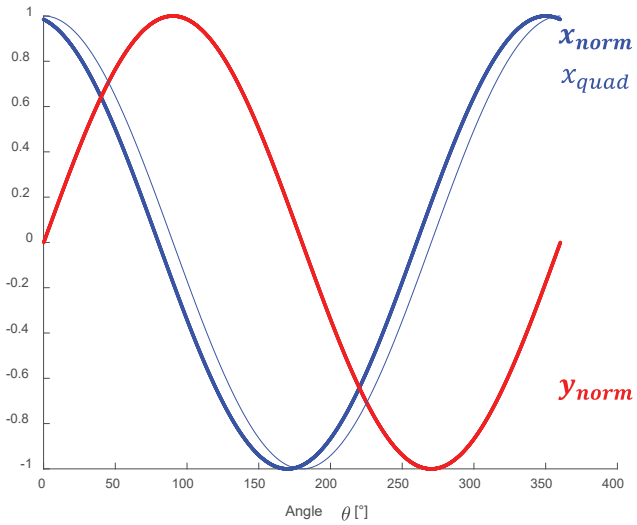
1. Impose quadrature between the two signals by phase-shifting one of the two signals:

$$x_{quad} = tan(\varphi_C - \varphi_S)\, y_{norm} + \frac{1}{cos(\varphi_C - \varphi_S)}\, x_{norm}$$

The pair of signals obtained can then be used to compute an angle value using an arctangent function. The resulting angle value includes a phase shift that must be removed:

$$\theta = \text{atan2D}(y_{norm}, x_{quad})$$

$$\theta = (\theta + \varphi_S) - \varphi_S$$




## Calculating Native Angle Error

Native Angle Error is meant to reflect the A33230's true angle performance without any external signal corrections. An example of calculating the Native Angle Error of the A33230 relative to an arbitrary reference angle, $\theta_{REF}$, can be seen as follows.

1. Angle is set to be $\theta_{REF}$, resulting in:

$$\begin{cases} x(\theta_{REF}) = A_c \cos(\theta_{REF} + \varphi_c) + O_c \\ y(\theta_{REF}) = A_s \sin(\theta_{REF} + \varphi_s) + O_s \end{cases}$$

2. Before performing the atan2(y,x) function, the x and y waveforms must be centered about 0. Subtracting the ideal $V_{OUT(Q)}$ value, $V_{CC}$ / 2, from each output will accomplish this without removing each output's $V_{OUT(Q)}$ errors.

$$\begin{cases} x_{norm} = x(\theta_{REF}) - \dfrac{V_{CC}}{2} \\ y_{norm} = y(\theta_{REF}) - \dfrac{V_{CC}}{2} \end{cases}$$



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3. Now the atan2(y,x) function can be used to solve for an angle value.

$$\theta_{NAT} = \text{atan2}(y_{norm}, x_{norm})$$

4. Finally, solve for the resulting Native Angle Error.

$$ERR_{ANG(NAT)\theta_{REF}} = \theta_{NAT} - \theta_{REF}$$

## Calculating Angle Micro-Linearity Error

Angle Micro-Linearity Error, $ERR_{\mu LIN(\theta)}$, is used to reflect the gradient of Native Angle Error over any 1° increment. For a single 1° step, $ERR_{\mu LIN(\theta)}$ can be solved by taking the report angle value at $ANG_{(\theta+1°)}$ and subtracting the angle value at $ANG_{(\theta)}$ + 1°. This is described in the following equation:

$$ERR_{\mu LIN(\theta)} = ANG_{(\theta_{REF}+1°)} - (ANG_{(\theta_{REF})} + 1°)$$

Conceptually, this is the same as taking the difference in Native Angle Error over any 1° increment.

## Calculating One-Time Corrected Angle Error

To improve Angle Accuracy relative to Native Angle Error, a one-time correction can be applied to each A33230 output. An End-of-Line (EOL) calibration at 25°C is required in this case to solve for the parameters $A_C$, $A_S$, $O_C$, $O_S$, $\varphi_C$, and $\varphi_S$. Once these parameters are solved for, they can be used to compensate the A33230's real-time output in-application. The equations outlined in the Offset, Amplitude, Phase Correction, and Angle Derivation section describe the necessary steps to achieve a corrected angle value.

## Calculating Dynamic Correction Angle Error

Offset, amplitude, and phase of the corrected sine and cosine waves will change with temperature, so using the compensation factors solved for at 25°C for all operating ranges will inject error into the system. To reduce Angle Error even further, an external system can apply an algorithm to dynamically adjust the offset ($O_C$, $O_S$) and amplitude ($A_C$, $A_S$) parameters in-application.

Once these parameters are solved for, they can be used to compensate the A33230's real-time output in-application. An example showing an external peak detector can be seen in the following section.

## Recommended External Peak Detector for Dynamic Correction

Implementing a simple peak detector algorithm can provide users with a method to dynamically correct offset and amplitude over temperature. This peak-detector will monitor the maximum and minimum amplitudes of the corrected sine and cosine waveforms throughout operation. When a change in amplitude or offset occurs, it can be dynamically removed after a recommended rotation of 270°. A summary of this process is described below.

1. 25°C calibration is performed to solve and compensate the native sine and cosine waveforms:

$$Offset\begin{cases} O_C = \dfrac{\max(x, 25°C) - \min(x, 25°C)}{2} \\ O_S = \dfrac{\max(y, 25°C) - \min(y, 25°C)}{2} \end{cases}$$

$$Amplitude\begin{cases} A_C = \dfrac{\max(x, 25°C) + \min(x, 25°C)}{2} \\ A_S = \dfrac{\max(y, 25°C) + \min(y, 25°C)}{2} \end{cases}$$

$$Normalize\begin{cases} x_{norm} = \dfrac{x - O_C}{A_C} \\ y_{norm} = \dfrac{y - O_S}{A_S} \end{cases}$$

$$\frac{Impose}{Quad}\left\{ x_{quad} = \tan(\varphi_C - \varphi_S)\, y_{norm} + \frac{1}{\cos(\varphi_C - \varphi_S)} x_{norm} \right.$$

$$Solve\ Angle\begin{cases} \theta - \varphi_S = atan2D(y_{norm}, x_{quad}) \\ \theta = (\theta - \varphi_S) - \varphi_S \end{cases}$$

2. Track the maximum and minimum values of the corrected sine and cosine waveforms in operation. Once a recommended 270° of rotation has occurred, recalculate the offset and amplitude compensation factors.

$$Offset\begin{cases} O_C = \dfrac{\max(x_{quad}) - \min(x_{quad})}{2} \\ O_S = \dfrac{\max(y_{norm}) - \min(y_{norm})}{2} \end{cases}$$

$$Amplitude\begin{cases} A_C = \dfrac{\max(x_{quad}) + \min(x_{quad})}{2} \\ A_S = \dfrac{\max(y_{norm}) + \min(y_{norm})}{2} \end{cases}$$

$$Normalize\begin{cases} x_{norm} = \dfrac{x_{quad} - O_C}{A_C} \\ y_{norm} = \dfrac{y_{norm} - O_S}{A_S} \end{cases}$$

$$\frac{Impose}{Quad}\left\{ x_{quad} = \tan(\varphi_C - \varphi_S)\, y_{norm} + \frac{1}{\cos(\varphi_C - \varphi_S)} x_{norm} \right.$$

$$Solve\ Angle\begin{cases} \theta - \varphi_S = atan2D(y_{norm}, x_{quad}) \\ \theta = (\theta - \varphi_S) - \varphi_S \end{cases}$$



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## PACKAGE OUTLINE DRAWING

**For Reference Only – Not for Tooling Use**

(Reference Allegro DWG-0000628, Rev. 1)
Dimensions in millimeters – NOT TO SCALE
Dimensions exclusive of mold flash, gate burrs, and dambar protrusions
Exact case and lead configuration at supplier discretion within limits shown

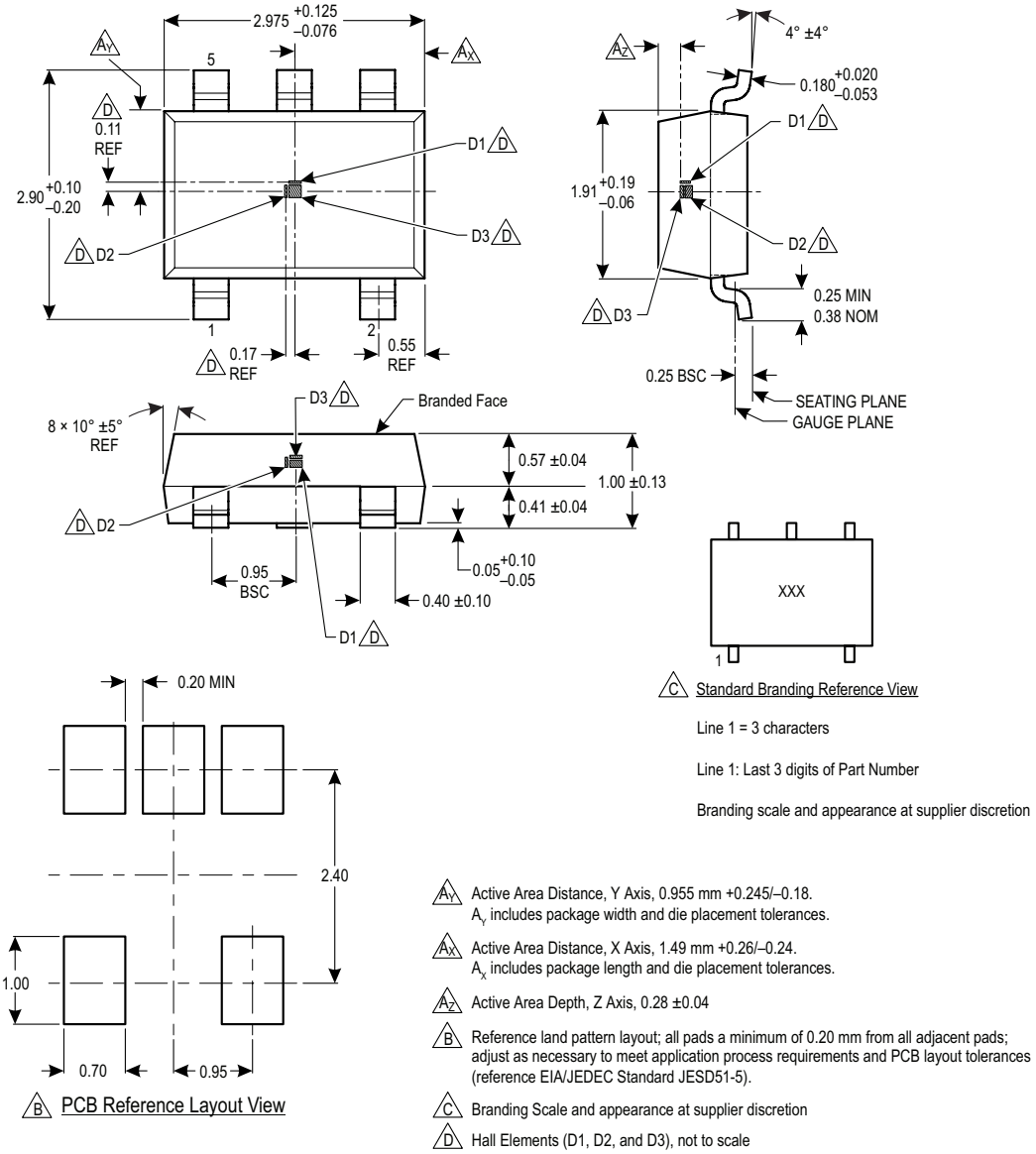



**Figure 18: Package LH, 5-Pin SOT23-W**



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## Revision History

| Number | Date | Description |
|---|---|---|
| – | November 17, 2021 | Initial release |
| 1 | December 1, 2021 | Removed Orthogonality Error footnote and Sample Refresh Rate characteristic (page 4); removed Angle Micro-Linearity Error footnote, Footnote 2 (page 5); updated Native Angle Error, One Time External Correction, and Dynamic External Correction values (page 5); updated Figures 7-10 (page 7); updated Calculating Angle Micro-Linearity Error section (page 13); updated package drawing notes $A_X$ and $A_Y$ (page 14). |
| 2 | January 17, 2022 | Updated Features and Benefits (page 1) and “Delay Time” to “Response Time” (page 4); corrected Native Angle Error, One Time External Correction, and Dynamic External Correction values (page 5) |

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